*Engineering Electromagnetics Essentials*

*Chapter 6*

*Wave equation and its solution for a wave propagating through an unbounded* 

*medium*



Study of propagation of uniform plane electromagnetic waves through unbounded media such as free-space and conducting media



Representation of a wave

Establishment of wave equations in electric and magnetic fields

Wave propagation through an unbounded free-space medium

Wave propagation through a resistive medium

Skin depth, surface resistance and ac resistance

Wave propagation through sea water and choice of operating frequency vis-à-vis attenuation

Wave propagation through a medium of charge particles

*Background*

Basic concepts of time-varying fields developed in Chapter 5 including Maxwell's equations

*Representation of a quantity associated with a wave*

A quantity that varies periodically with space and time is said to be associated with a wave. Let us see how a mathematical function can represent a propagating wave.

Let us examine the function

 $\overline{\phantom{a}}$  $\int$  $\setminus$  $\mathbf{r}$  $\setminus$  $\bigg($  $\int_{+}^{1} (t, z) = f_{+} | t$ *v z*  $f_{+}(t, z) = f_{+} | t$ provided  $\Delta t - \Delta t = 0$  (condition)  $(\Delta t - \frac{\Delta z}{\Delta t})$  =  $f_+(t - \frac{2}{\Delta t})$  $(t + \Delta t, z + \Delta z) = f_{+} \vert t + \Delta t - \frac{z + \Delta z}{\Delta z} \vert$  $\Delta$  $\Delta t-$ J  $\setminus$  $\overline{\phantom{a}}$  $\setminus$  $\int_{t_1}^{t_2} Z_{t_1}(\Lambda_t) \Delta$  $= f_{+} \left( t - \frac{2}{v} + (\Delta t - \frac{\Delta z}{v}) \right) = f_{+} \left( t - \frac{2}{v} \right)$ J  $\setminus$  $\mathsf{I}$  $\setminus$  $\int_{t_1}$   $z + \Delta$  $\int_{+}^{1} (t + \Delta t, z + \Delta z) = f_{+} \left( t + \Delta t - \frac{z + \Delta z}{v} \right)$ *v z t z*  $f_{_+}(t)$ *v z t v z*  $f_{\scriptscriptstyle +}|$  t *z z*  $f_{+}(t+\Delta t, z+\Delta z) = f_{+}|t+\Delta t$ *t z v*  $\Delta$  $\Delta$ = (condition)  $0 \Delta t$  dt *dz t z t Lt*  $v = \frac{v}{\sqrt{2}} =$  $\Delta$  $\Delta$  $\Delta t \rightarrow$ = direction

Subscript + refers to a forward wave propagating in positive z



*v* is identified as the velocity of wave.

Thus the function

$$
f_+(t,z) = f_+\left(t - \frac{z}{v}\right)
$$

represents a forward wave propagating in positive z direction

Similarly, now let us examine the function

$$
f_{-}(t, z) = f_{-}\left(t + \frac{z}{v}\right)
$$
  
\n
$$
= f_{-}\left(t + \Delta t, z - \Delta z\right) = f_{-}\left(t + \Delta t + \frac{z - \Delta z}{v}\right)
$$
  
\n
$$
= f_{-}\left(t - \frac{z}{v} + (\Delta t - \frac{\Delta z}{v})\right) = f_{-}(t + \frac{z}{v})
$$
  
\nprovided  $\Delta t - \frac{\Delta z}{v} = 0$  (condition)  
\n
$$
= \frac{Lt}{\Delta t}
$$
  
\n
$$
v = \frac{Lt}{\Delta t} \frac{\Delta z}{dt} = \frac{dz}{dt}
$$
 (condition)

*v* is identified as the velocity of wave.

# Thus the function

$$
f_{-}(t,z) = f_{-}\left(t + \frac{z}{v}\right)
$$

represents a backward wave propagating in negative z direction

## We have thus seen that

the function

 $\overline{\phantom{a}}$  $\int$  $\backslash$  $\overline{\phantom{a}}$  $\setminus$ ſ  $\int_{+}^{1} (t, z) = f_{+} | t$ *v z*  $f_{+}(t, z) = f_{+} | t$ 

represents a forward wave propagating in positive z direction

## and that

# the function

$$
f_{-}(t,z) = f_{-}\left(t + \frac{z}{v}\right)
$$

represents a backward wave propagating in negative z direction

How to choose the functions so that they can represent the periodicity of the wave with space and tome coordinates?

Choose the functions as proportional to exp *j(t-z/v)* for a forward wave and to exp *j(* $\omega t$ *+z/v)* for a backward wave in phasor notation?

Choose the functions as proportional to exp *j(t-z/v)* for a forward wave and to  $\exp j(\omega t + z/v)$  for a backward wave in phasor notation.

 $\overline{\phantom{a}}$ Į  $\setminus$  $\mathbf{r}$  $\setminus$  $\bigg($  $\int_{+}^{1} (t, z) = f_{+} | t$ *v z*  $f_{+}(t, z) = f_{+} | t$  $\overline{\phantom{a}}$  $\backslash$  $\overline{\phantom{a}}$ ſ  $\int_{-}^{1} (t, z) = f_{-} \vert t +$ *z*  $f_{-}(t, z) = f_{-}|t$ 

 $\setminus$ 

(forward wave)

(backward wave)

Phasor is a rotating vector

 $\int$ 

*v*

Phasor diagram of a time-periodic quantity, say magnitude of electric field  $E$  of amplitude  $\ E_{0}$  rotating with angular velocity  $\omega$ 

With reference to physical quantity, say, electric field for forward and backward waves, we may take the functions taking into regard their periodicity as follows:

$$
E_{+} = E_0 \exp(j\omega t') = E_0 \exp j\omega(t - z/v)
$$

interpreting *t* in phasor notation *t* / as

$$
t' = t - z / v
$$
 (forward wave)

## and

$$
E_{-} = E_0 \exp j\omega t'' = E_0 \exp j\omega(t + z/v)
$$

interpreting *t* in phasor notation *t <sup>i</sup>*/ as

 $t'' = t + z/v$  (backward wave)





In an alternative approach, we can choose either the real or imaginary part of the function to represent the wave. Taking the real part:

$$
E_{+} = E_{0} \cos \omega (t - z/v)
$$
 (forwardwave)  
\n
$$
E_{-} = E_{0} \cos \omega (t + z/v)
$$
 (backwardwave)  
\n
$$
\omega (t - z/v) = \omega t - (\omega/v) z = \omega t - \beta z
$$
\n= phase of the forward wave  
\n
$$
\omega (t + z/v) = \omega t + (\omega/v) z = \omega t + \beta z
$$
\nPhase of the wave determines (i) the value of the quantity (here, typically,  
\n
$$
\omega (t + z/v) = \omega t + (\omega/v) z = \omega t + \beta z
$$
\n= phase of the backward wave  
\n= phase of the backward wave  
\n
$$
= \frac{\omega}{\omega}
$$

*Wave phase velocity, wavelength and frequency and the relation between them*

 $\omega t - \beta z$  = phase of the forward wave (recalled)

Put the phase of the wave as constant:

phase= $\omega t - \beta z$  = constant  $\begin{tabular}{|c|c|} \hline \quad \leftarrow & \text{Differentiating} \end{tabular}$  $\beta$  $=\frac{\omega}{\omega}$ *dt dz*  $\beta$  $v_{\rm ph} = \frac{\omega}{\rho}$  (phase velocity of the wave) velocity of the constant phase of the wave

Variation of the quantity (here, electric field magnitude) representing a wave, typically, forward wave, with space coordinate z at a fixed time (snap-shot), typically *t* = 0:

$$
E_{+} = E_{0} \cos(\omega t - \beta z)
$$
  
\n
$$
\leftarrow t = 0 \text{ (at a fixed time)}
$$
  
\n
$$
E_{+} = E_{0} \cos(-\beta z) = E_{0} \cos \beta z
$$

 $\frac{1}{2} \cos(\omega t - \beta z)$ <br>  $\leftarrow$   $t = 0$  (at a fixed time) (recalled)<br>  $\frac{1}{2} \cos(\omega t - \beta z) = E_0 \cos \beta z$   $\leftarrow$  Positive maximum  $\rightarrow \cos \beta z = 1$ <br>  $\frac{1}{2} \cos(\omega t - \beta z) = E_0 \cos \beta z$   $\leftarrow$  Positive maximum value of the quantity)<br>  $\frac{1}{2} \cos(\omega t - \$  $E_{+} = E_0 \cos(\omega t - \beta z)$  $E_+ = E_0 \cos(-\beta z) = E_0 \cos \beta z$   $\longleftrightarrow$  Positive maximum  $\rightarrow \cos \beta z = 1$  $t = 0$  (at a fixed time) (recalled)  $\beta z$  =  $0, 2\pi, 4\pi, 6\pi, ...$  (corresponding to the same phase: here, referring to positive maximum value of the quantity) Interval of  $\beta z$  between two consecutive same phases at a fixed time  $\beta z = 2\pi$  $\beta$  $2\pi$ *z* = Distance between two consecutive same phases at a fixed time called wavelength  $\lambda$  $\beta$  $\lambda = \frac{2\pi}{\sqrt{2}}$  $=\frac{2\pi}{2}$  (wavelength)  $E_{+} = E_{0}$  $\lambda$  $\beta = \frac{2\pi}{\lambda}$ 2  $=\frac{2\pi}{4}$  (wave propagation constant)

$$
E_{+} = E_{0} \cos(\omega t - \beta z)
$$
\n
$$
+ z = 0 \text{ (at a fixed distance)}
$$
\n
$$
E_{+} = E_{0} \cos \omega t
$$
\n
$$
+ \text{Positive maximum} \rightarrow \cos \omega t = 1
$$
\n
$$
E_{+} = E_{0}
$$
\n
$$
= 0, 2\pi, 4\pi, 6\pi, ... \text{ (corresponding to the same phase: here, referring to positive maximum value of the quantity)}
$$
\n
$$
= 2\pi \text{ Time interval between two consecutive same phases at a fixed distance called time period } T
$$
\n
$$
t = \frac{2\pi}{\omega} \text{ Time interval between two consecutive same phases at a fixed distance called time period } T
$$
\n
$$
t = \frac{2\pi}{\omega} \text{ Time interval between two consecutive same phases at a fixed distance}
$$

$$
T = \frac{2\pi}{\omega}
$$
\n
$$
f = \frac{1}{T} = \frac{\omega}{2\pi}
$$
 (wave circular frequency or simply frequency)  
\n
$$
\omega = 2\pi f
$$
 (wave circular frequency or simply frequency)  
\n
$$
v_{\text{ph}} = \frac{2\pi f}{\beta} \leftarrow \beta = \frac{2\pi}{\lambda}
$$
\n
$$
v_{\text{ph}} = f\lambda
$$
 (relation between phase velocity, frequency and wavelength)

*Wave equations in electric and magnetic fields*

*Wave equation in electric field*

Electric and magnetic fields are coupled in the following two Maxwell's equations:

$$
\nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t}
$$
  
\n
$$
\nabla \times \vec{H} = \vec{J} + \varepsilon \frac{\partial \vec{E}}{\partial t}
$$
 (Maxwell's equations recalled)

read it using the second of these equations. In order to decouple these two equations to obtain a single equation, namely wave equation in electric field, take the curl operation on the first of these equations and

$$
\nabla \times \nabla \times \vec{E} = -\mu \nabla \times \frac{\partial \vec{H}}{\partial t}
$$

 $\int$ 

=

 $\ddot{B} = \mu H$ 

 $\mu$ 

 $\mathcal E$ 

=

 $\ddot{D} = \varepsilon \dot{E}$  $\rightarrow$   $\rightarrow$ 

 $\rightarrow$ 

 $\overline{a}$  $\left\{ \right.$  $\mathbf{I}$ 

$$
\nabla \times \nabla \times \vec{E} = -\mu \nabla \times \frac{\partial \vec{H}}{\partial t} \text{ (rewritten)} \longleftarrow \text{Partial time derivative and curl involving partial derivatives in space coordinates are interchangeable}
$$
\n
$$
\nabla \times \nabla \times \vec{E} = -\mu \frac{\partial}{\partial t} (\nabla \times \vec{H}) \longleftarrow \nabla \times \vec{H} = \vec{J} + \varepsilon \frac{\partial \vec{E}}{\partial t} \text{ (Maxwell's equation)}
$$
\n
$$
\nabla \times \nabla \times \vec{E} = -\mu \frac{\partial}{\partial t} (\vec{J} + \varepsilon \frac{\partial \vec{E}}{\partial t}) = -\mu \frac{\partial \vec{J}}{\partial t} - \mu \varepsilon \frac{\partial^2 \vec{E}}{\partial t^2}
$$
\n
$$
\nabla \times \nabla \times \vec{E} = \nabla (\nabla \cdot \vec{E}) - \nabla^2 \vec{E}
$$
\n
$$
\nabla (\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = -\mu \frac{\partial \vec{J}}{\partial t} - \mu \varepsilon \frac{\partial^2 \vec{E}}{\partial t^2}
$$
\n
$$
\nabla \cdot \vec{E} = \frac{\rho}{\varepsilon} \text{ (Maxwell's equation)}
$$
\n
$$
\downarrow \nabla^2 \vec{E} - \mu \varepsilon \frac{\partial^2 \vec{E}}{\partial t^2} = \nabla (\frac{\rho}{\varepsilon}) + \mu \frac{\partial \vec{J}}{\partial t} \text{ (wave equation in electric field)}
$$
\n
$$
\nabla^2 \vec{E} - \mu \varepsilon \frac{\partial^2 \vec{E}}{\partial t^2} = \nabla (\frac{\rho}{\varepsilon}) + \mu \frac{\partial \vec{J}}{\partial t} \text{ (wave equation in electric field)}
$$

*Wave equation in magnetic field*

$$
\nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t}
$$
 (Maxwell's equations recalled)  

$$
\nabla \times \vec{H} = \vec{J} + \varepsilon \frac{\partial \vec{E}}{\partial t}
$$

In order to decouple these two equations to obtain a single equation, namely wave equation in magnetic field, take the curl operation on the second of these equations and read it using the first of these equations.

$$
\nabla \times \nabla \times \vec{H} = \nabla \times (\vec{J} + \varepsilon \frac{\partial \vec{E}}{\partial t}) = \nabla \times \vec{J} + \varepsilon \nabla \times \frac{\partial \vec{E}}{\partial t})
$$
\n
$$
\downarrow \qquad \qquad \downarrow \qquad \qquad \downarrow
$$
\n
$$
\nabla \times \nabla \times \vec{H} = \nabla \times \vec{J} + \varepsilon \frac{\partial}{\partial t} (\nabla \times \vec{E}) \qquad \qquad \nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t} \quad \text{(Maxwell's equation)}
$$
\n
$$
\downarrow \qquad \qquad \downarrow
$$
\n
$$
\nabla \times \nabla \times \vec{H} = \nabla \times \vec{J} - \mu \varepsilon \frac{\partial^2 \vec{H}}{\partial t^2}
$$
\n
$$
\qquad \qquad \downarrow
$$
\n
$$
\downarrow
$$

$$
\nabla \times \nabla \times \vec{H} = \nabla \times \vec{J} - \mu \varepsilon \frac{\partial^2 \vec{H}}{\partial t^2}
$$
\n
$$
\nabla (\nabla \cdot \vec{H}) - \nabla^2 \vec{H} = \nabla \times \vec{J} - \mu \varepsilon \frac{\partial^2 \vec{H}}{\partial t^2}
$$
\n
$$
\nabla (\nabla \cdot \vec{H}) - \nabla^2 \vec{H} = \nabla \times \vec{J} - \mu \varepsilon \frac{\partial^2 \vec{H}}{\partial t^2}
$$
\n
$$
\nabla^2 \vec{H} - \mu \varepsilon \frac{\partial^2 \vec{H}}{\partial t^2} = -\nabla \times \vec{J} \quad \text{(wave equation in magnetic field)}
$$
\n
$$
\nabla^2 \vec{E} - \mu \varepsilon \frac{\partial^2 \vec{E}}{\partial t^2} = \nabla \left( \frac{\rho}{\varepsilon} \right) + \mu \frac{\partial \vec{J}}{\partial t}
$$
\n
$$
\nabla^2 \vec{E} - \mu \varepsilon \frac{\partial^2 \vec{E}}{\partial t^2} = -\nabla \times \vec{J}
$$
\n
$$
\nabla^2 \vec{H} - \mu \varepsilon \frac{\partial^2 \vec{H}}{\partial t^2} = -\nabla \times \vec{J}
$$
\n
$$
\nabla^2 \vec{H} - \mu \varepsilon \frac{\partial^2 \vec{E}}{\partial t^2} = 0
$$
\n
$$
\nabla^2 \vec{H} - \mu \varepsilon \frac{\partial^2 \vec{E}}{\partial t^2} = 0
$$
\n
$$
\nabla^2 \vec{H} - \mu \varepsilon \frac{\partial^2 \vec{H}}{\partial t^2} = 0
$$
\n
$$
\nabla^2 \vec{H} - \mu \varepsilon \frac{\partial^2 \vec{H}}{\partial t^2} = 0
$$
\n
$$
\text{(source-free wave equations in electric and magnetic fields)} (\rho = \vec{J} = 0)
$$

# Consider a uniform plane wave propagating through an unbounded free-space medium.

$$
\nabla^2 \vec{E} - \mu \varepsilon \frac{\partial^2 \vec{E}}{\partial t^2} = 0
$$

$$
\nabla^2 \vec{H} - \mu \varepsilon \frac{\partial^2 \vec{H}}{\partial t^2} = 0
$$

(source-free wave equations in electric and magnetic fields)  $(\rho\!=\!\vec{J}\!=\!0)$ 



A plane wave has a plane wavefront. A wave front is an equi-phase surface over which the phase of the quantity associated with the wave remains constant. For a uniform plane wave, in addition to the phase, the amplitude of the quantity associated with the wave also remains constant over the plane wavefront.

Formulate the problem by considering wave

propagation along z in the rectangular coordinate system.

$$
\left.\frac{\partial^2 E_y}{\partial t^2}\right\} \leftarrow \nabla^2 \vec{E} - \mu \varepsilon \frac{\partial^2 \vec{E}}{\partial t^2} = 0
$$

$$
\nabla^2 H_x = \mu_0 \varepsilon_0 \frac{\partial^2 H_x}{\partial t^2}
$$
\n
$$
\nabla^2 H_y = \mu_0 \varepsilon_0 \frac{\partial^2 H_y}{\partial t^2}
$$
\n
$$
\nabla^2 H_z = \mu_0 \varepsilon_0 \frac{\partial^2 H_z}{\partial t^2}
$$
\n
$$
\nabla^2 H_z = \mu_0 \varepsilon_0 \frac{\partial^2 H_z}{\partial t^2}
$$

$$
\nabla^2 E_x = \mu_0 \varepsilon_0 \frac{\partial^2 E_x}{\partial t^2}
$$
\n
$$
\nabla^2 E_y = \mu_0 \varepsilon_0 \frac{\partial^2 E_y}{\partial t^2}
$$
\n
$$
\nabla^2 E_z = \mu_0 \varepsilon_0 \frac{\partial^2 E_z}{\partial t^2}
$$

$$
\frac{\partial^2 E_x}{\partial x^2} + \frac{\partial^2 E_x}{\partial y^2} + \frac{\partial^2 E_x}{\partial z^2} = \mu_0 \varepsilon_0 \frac{\partial^2 E_x}{\partial t^2}
$$
\n
$$
\frac{\partial^2 E_y}{\partial x^2} + \frac{\partial^2 E_y}{\partial y^2} + \frac{\partial^2 E_y}{\partial z^2} = \mu_0 \varepsilon_0 \frac{\partial^2 E_y}{\partial t^2}
$$
\n
$$
\frac{\partial^2 E_z}{\partial x^2} + \frac{\partial^2 E_z}{\partial y^2} + \frac{\partial^2 E_z}{\partial z^2} = \mu_0 \varepsilon_0 \frac{\partial^2 E_z}{\partial t^2}
$$

$$
\nabla^2 H_x = \mu_0 \varepsilon_0 \frac{\partial^2 H_x}{\partial t^2}
$$
  

$$
\nabla^2 H_y = \mu_0 \varepsilon_0 \frac{\partial^2 H_y}{\partial t^2}
$$
  

$$
\nabla^2 H_z = \mu_0 \varepsilon_0 \frac{\partial^2 H_z}{\partial t^2}
$$

 $\mathbf{I}$ 

$$
\frac{\partial^2 H_x}{\partial x^2} + \frac{\partial^2 H_x}{\partial y^2} + \frac{\partial^2 H_x}{\partial z^2} = \mu_0 \varepsilon_0 \frac{\partial^2 H_x}{\partial t^2}
$$
\n
$$
\frac{\partial^2 H_y}{\partial x^2} + \frac{\partial^2 H_y}{\partial y^2} + \frac{\partial^2 H_y}{\partial z^2} = \mu_0 \varepsilon_0 \frac{\partial^2 H_y}{\partial t^2}
$$
\n
$$
\frac{\partial^2 H_z}{\partial x^2} + \frac{\partial^2 H_z}{\partial y^2} + \frac{\partial^2 H_z}{\partial z^2} = \mu_0 \varepsilon_0 \frac{\partial^2 H_z}{\partial t^2}
$$

For a uniform plane wave propagating along z



(wave equation in electric field for a uniform plane wave in free space)

(wave equation in magnetic field for a uniform plane wave in free space)

$$
\nabla \cdot \vec{E} = 0 \quad \leftarrow \quad \nabla \cdot \vec{E} = \frac{\rho}{\varepsilon} \text{ (Maxwell's equation)} \qquad \nabla \cdot \vec{H} = 0 \text{ (Maxwell's equation)}
$$
\n
$$
\rho = 0 \qquad \text{for a free-space medium}
$$
\n
$$
\frac{\partial E_x}{\partial x} + \frac{\partial E_y}{\partial y} + \frac{\partial E_z}{\partial z} = 0 \qquad \leftarrow \quad \frac{\partial}{\partial x} = \frac{\partial}{\partial y} = 0 \qquad \rightarrow \quad \frac{\partial H_x}{\partial x} + \frac{\partial H_y}{\partial y} + \frac{\partial H_z}{\partial z} = 0
$$
\n
$$
\frac{\partial E_z}{\partial z} = 0 \qquad \qquad \text{for a uniform plane wave}
$$
\n
$$
\frac{\partial E_z}{\partial z} = 0 \qquad \qquad E_z \text{ and } H_z \text{ are each constant}
$$
\n
$$
\text{with z}
$$
\n
$$
\frac{\partial^2 E_z}{\partial z^2} = 0 \qquad \rightarrow \quad \frac{\partial^2 E_z}{\partial z^2} = \mu_0 \varepsilon_0 \frac{\partial^2 E_z}{\partial z^2} \qquad \frac{\partial^2 H_z}{\partial z^2} = \mu_0 \varepsilon_0 \frac{\partial^2 H_z}{\partial t^2} \qquad \leftarrow \quad \frac{\partial^2 H_z}{\partial z^2} = 0
$$
\n
$$
\frac{\partial^2 E_z}{\partial t^2} = 0 \qquad \qquad \frac{\partial^2 H_z}{\partial t^2} = 0
$$

20



A uniform plane wave propagating through an unbounded free-space medium is essentially a transverse electromagnetic wave (TEM) with no electric and magnetic field components in the direction of propagation (along z)

$$
\nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t}
$$
\n
$$
\nabla \times \vec{H} = \vec{J} + \varepsilon \frac{\partial \vec{E}}{\partial t}
$$
\n(Maxwell's equations recalled)  
\n
$$
\nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t}
$$
\n
$$
\nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t}
$$
\n
$$
\nabla \times \vec{H} = \varepsilon \frac{\partial \vec{E}}{\partial t}
$$
\n
$$
\nabla \times \vec{H} = \varepsilon \frac{\partial \vec{E}}{\partial t}
$$
\n
$$
\nabla \times \vec{H} = \varepsilon \frac{\partial \vec{E}}{\partial t}
$$
\n
$$
E_z = 0
$$
\n
$$
H_z = 0
$$
\n
$$
\frac{\partial E_y}{\partial z} \vec{a}_x + \frac{\partial E_x}{\partial z} \vec{a}_y = -\mu_0 \frac{\partial}{\partial t} (H_x \vec{a}_x + H_y \vec{a}_y)
$$
\n
$$
= \frac{\partial H_y}{\partial z} \vec{a}_x + \frac{\partial H_x}{\partial z} \vec{a}_y = \varepsilon_0 \frac{\partial}{\partial t} (E_x \vec{a}_x + E_y \vec{a}_y)
$$
\nEquating the x-components and y-components of the left- and right-hand sides\n
$$
\frac{\partial E_y}{\partial z} = \mu_0 \frac{\partial H_x}{\partial t}
$$
\n
$$
\frac{\partial E_x}{\partial z} = -\mu_0 \frac{\partial H_y}{\partial t}
$$
\n
$$
\frac{\partial H_x}{\partial z} = \varepsilon_0 \frac{\partial E_x}{\partial t}
$$
\n
$$
\frac{\partial H_x}{\partial z} = \varepsilon_0 \frac{\partial E_y}{\partial t}
$$
\n22

 $\mathbf{I}$  $\overline{ }$  $\int$ 

 $\partial$ 

*H*

*t*

= −

 $x = 1, y = 0$ 

 $\mu_{\scriptscriptstyle 0}$ 

 $\partial$ 

*z*

*E*

 $\partial$ 

 $\mathbf{I}$  $\overline{ }$  $\int$ 

 $\partial$ 

*E*

*t*

 $\partial$ 

 $x = c \frac{U E_y}{V}$ 

 $\mathcal{E}^{}_0$ 

=

 $\partial$ 

*H*

*z*

 $\partial$ 



23

$$
\vec{E} \cdot \vec{H} = 0
$$

$$
\frac{\omega}{\beta} = v_{\text{ph}} = \frac{1}{\sqrt{\mu_0 \varepsilon_0}} = c
$$

Unbounded free-space medium supports transverse electromagnetic (TEM) wave, such that the directions of the electric field, magnetic field and propagation are mutually perpendicular to one another, propagating with phase velocity equal to the speed of light *c:*

$$
\mu_0 = 4\pi \times 10^{-7} \text{ H/m}
$$
  $\rightarrow c = \frac{1}{\sqrt{\mu_0 \varepsilon_0}} = 3 \times 10^8 \text{ m/s}$   $\leftarrow$   $\varepsilon_0 = 1/(36\pi) \times 10^{-9} = 8.854 \times 19^{-12} \text{ F/m}$ 

Intrinsic impedance  $\eta_0$  of the free-space medium is

$$
\frac{E_x}{H_y} = -\frac{E_y}{H_x} = \frac{\omega \mu_0}{\beta}
$$
\n
$$
\eta_0 = \frac{E}{H} = \frac{(E_x^2 + E_y^2)^{1/2}}{(H_x^2 + H_y^2)^{1/2}}
$$
\n
$$
\eta_0 = \frac{(E_x^2 + E_y^2)^{1/2}}{(H_x^2 + H_y^2)^{1/2}} = \frac{\left[\left(\frac{\omega \mu_0}{\beta}\right)^2 (H_x^2 + H_y^2)\right]^{1/2}}{(H_x^2 + H_y^2)^{1/2}} = \frac{\omega \mu_0}{\beta}
$$

10

$$
\eta_0 = \frac{\omega \mu_0}{\beta} \text{ (rewritten)} \longleftrightarrow \beta = \omega \sqrt{\mu_0 \varepsilon_0} \longleftrightarrow \beta^2 = \omega^2 \mu_0 \varepsilon_0
$$
  
\n
$$
\downarrow \qquad \qquad \mu_0 = 4\pi \times 10^{-7} \text{ H/m}
$$
  
\n
$$
\eta_0 = \sqrt{\frac{\mu_0}{\varepsilon_0}} = 120\pi
$$
  
\n
$$
\eta_0 = \sqrt{\frac{\mu_0}{\varepsilon_0}} = 120\pi
$$
  
\n(intrinsic impedance of a free-space medium) (intrinsic impedance of a free-space medium)

(intrinsic impedance of a free-space medium)

 $\mathcal{E}^{}_0$ 

*Wave propagation through a conducting medium*

Let us recall wave equation in electric field:

2 2 2 *t J t E E*  $\partial$  $\partial$  $|+$  $\int$  $\backslash$  $\mathbf{I}$  $\setminus$ ſ  $=\nabla$  $\partial$  $\partial$  $\nabla^2 \vec{E}$  –  $\rightarrow$   $\rightarrow$   $\rightarrow$  $\rightarrow$  $\mu$  $\mathcal E$  $\rho$  $\mu \varepsilon \frac{\partial}{\partial x^2} = \nabla \left| \frac{\partial}{\partial x} \right| + \mu \frac{\partial}{\partial x}$  (recalled) (wave equation in electric field) 2 2 2 *t E t E E*  $\partial$  $\partial$ +  $\partial$  $\partial$  $\nabla^2 \vec{E} =$  $\rightarrow$   $\rightarrow$  $\rightarrow$  $\mu\sigma = + \mu\epsilon$  (conducting medium) 0  $\int$  $\left\{ \right.$  $\vert$ = =  $J = \sigma E$  $\rightarrow$   $\rightarrow$  $\sigma$  $\rho$  $\mathbf{I}$  $\overline{ }$  $\int$  $\overline{\phantom{a}}$  $\left\{ \right.$  $\vert$  $\equiv (j\omega)(j\omega) = \partial$  $\partial$  $\equiv$  $\partial$  $\partial$ 2 2 2  $(j\omega)(j\omega) = -\omega$  $\omega$  $j\omega$ ) $(j$ *t j t*  $\vec{E}$  =  $j\omega\mu$   $(\sigma + j\omega\varepsilon)\vec{E}$   $\nabla^2 \vec{E} = j \omega \mu \ (\sigma + j \omega \varepsilon) \vec{E}$   $\longleftarrow$   $\gamma = \sqrt{j \omega \mu \ (\sigma + j \omega \varepsilon)}$  $\vec{E} = \gamma^2 \vec{E}$  $\nabla^2 \vec{E} = \gamma^2 \vec{E}$ 

 $\nabla^2 \vec{E} = \gamma^2 \vec{E}$ 



 $\int$  $\beta$  = phase propagation constant of the wave  $\mathcal{L}$  $\alpha$  = attenuation constant of the wave



$$
E_x = E_{x0} \exp[-(\alpha + j\beta)z] = E_{x0} \exp(-\alpha z) \exp(-j\beta z)
$$
  

$$
E_y = E_{y0} \exp[-(\alpha + j\beta)z] = E_{y0} \exp(-\alpha z) \exp(-j\beta z)
$$

)<br>J  $\left\{ \right.$  $\vert$  $\beta$  = phase propagation constnat of the wave  $\alpha$  = attenuation constant of the wave Invoking time dependence exp(*jat*)

$$
E_x = E_{x0} \exp[-(\alpha + j\beta)z] = E_{x0} \exp(-\alpha z) \exp(-j\beta z) \exp(j\omega t)
$$
  
\n
$$
E_y = E_{y0} \exp[-(\alpha + j\beta)z] = E_{y0} \exp(-\alpha z) \exp(-j\beta z) \exp(j\omega t)
$$

Amplitude exponentially attenuates as  $\exp(-\alpha z)$ 

$$
\gamma = \sqrt{j\omega\mu(\sigma + j\omega\varepsilon)} = \alpha + j\beta \quad \text{(recalled)}
$$
\n
$$
\downarrow \qquad \qquad \text{For a good conductor:}
$$
\n
$$
\gamma = \sqrt{j\omega\mu\sigma} = \alpha + j\beta \qquad \qquad \sigma \gg \omega\varepsilon
$$



(for a good conductor)  $(\sigma \gg \omega \varepsilon)$ 

$$
\alpha = \beta = \sqrt{\frac{\omega \mu_0 \sigma}{2}}
$$
  
(for a good conductor)  $(\sigma >> \omega \varepsilon)$   

$$
E_x = E_{x0} \exp[-(\alpha + j\beta)z] = E_{x0} \exp(-\alpha z) \exp(-j\beta z) \exp(j\omega t)
$$
  

$$
E_y = E_{y0} \exp[-(\alpha + j\beta)z] = E_{y0} \exp(-\alpha z) \exp(-j\beta z) \exp(j\omega t)
$$

Amplitude exponentially attenuates as  $\exp(-\alpha z)$ 

Taking  $\alpha$  = 1/ $\delta$ , the exponential attenuating factor of the field amplitude may be put as

$$
\exp(-\alpha z) = \exp(-z/\delta)
$$

Putting  $z = \delta$ , we appreciate that the field amplitude at the surface (skin) of a good conductor at *z* = 0 attenuates by a factor of exp (-1) = 1/*e* at a depth equal to  $z = \delta$  called the skin depth of the conductor.

$$
\alpha = 1/\delta
$$
\n
$$
\downarrow
$$
\n
$$
\delta = 1/\alpha \qquad \leftarrow \qquad \alpha = \sqrt{\frac{\omega \mu_0 \sigma}{2}}
$$
\n
$$
\delta = \sqrt{\frac{2}{\omega \mu_0 \sigma}} \qquad \text{(skin depth)}
$$

$$
\delta = \sqrt{\frac{2}{\omega\mu_0 \sigma}}
$$
 (skin depth)  $\leftarrow \omega = 2\pi f$   
\n
$$
\delta = \sqrt{\frac{1}{\pi f \mu_0 \sigma}}
$$
 **Skin depth decreases with the increase of the conductivity of the medium and operating frequency**  
\n
$$
\alpha = \beta = \sqrt{\frac{\omega\mu_0 \sigma}{2}} \quad (\sigma >> \omega \varepsilon)
$$
\n
$$
\beta = 2\pi / \lambda
$$
\n
$$
\delta = \frac{1}{\beta} = \frac{\lambda}{2\pi}
$$
 **Skin depth is directly proportional to the wavelength in the conducting medium.**

Typically, for copper ( $\sigma$  = 5.8x10<sup>7</sup> mho/m), at operating frequency 50 Hz, the value of the skin depth is  $\sim$  9.4 mm.

The skin depths are  $\sim$  2.1 mm,  $\sim$  66.1  $\mu$  m, and  $\sim$  2.1  $\mu$  m, for frequencies 1 kHz, 1 MHz, and 1 GHz, respectively. For 10 GHz frequency, we find the skin depth as 6.61x10<sup>-7</sup> m, which happens to be in the range of wavelength of visible light.





Let us recall the expression for electric field intensity at depth *z* from the surface of the conductor:

 $E_y = E_{y0} \exp{-\left(\alpha + j\beta\right)z}$  (recalled) (RF time dependence *jat* understood)  $E_y = E_{y0} \exp{-\left(\alpha + j\beta\right)z\exp(j\omega t)}$ 

 $E_{\mathrm{\,y0}}$  =  $\,$  Electric field intensity amplitude at the surface of the conductor  $\,$ 

Current density along *y* at depth *z* from the surface of the conductor

$$
= \sigma E_{y0} \exp{-\left(\alpha + j\beta\right)z}
$$

Current through the strip of infinitesimal thickness *dz* and width *W*

 $=[\sigma E_{y0} \exp-(\alpha + j\beta)z][Wdz]$ 

Current through the entire conductor of width *W*

$$
= \int_{0}^{\infty} \sigma WE_{y0} \exp(-(\alpha + j\beta)) dz
$$
  
=  $\sigma WE_{y0} \left[ \frac{\exp(-(\alpha + j\beta))z}{-(\alpha + j\beta)} \right]_{0}^{\infty} = \frac{\sigma WE_{y0}}{\alpha + j\beta}$ 

Current through the entire conductor of unit width (*W* = 1)

$$
=\frac{\sigma E_{y0}}{\alpha + j\beta}
$$



## Surface impedance *Zs* is defined as



# **ac resistance of a straight conducting wire:**

We can find the ac resistance of a straight round wire (that is, of circular cross section) made of a good conductor at high frequencies and compare it with its dc resistance to show that the ac-to-DC resistance ratio of the wire is a/2 $\delta$ , where a is the radius of the wire and  $\delta$  is the skin depth of the conductor making the wire.

Expression for the dc resistance  $R_{dc}$  of a wire of length *l* and radius *a* is well known:

$$
R_{\rm dc} = \frac{1}{\sigma} \frac{l}{\pi a^2}
$$

Let us next proceed to find an expression for the ac resistance *R*<sub>ac</sub> of the wire using the same approach as used to find the surface resistance.

For a round wire of radius a large compared to the skin depth  $\delta$ , a point inside the wire where the electric field is significant will not 'see' the curvature of the round wire and therefore we can take the surface of the wire as a planar surface.

Therefore, following exactly the same approach as used to find the surface resistance of a planar conductor we can find the resistance of the round wire interpreting the width as the circumference of the wire ( $W = 2\pi a$ ).



the imaginary part  $X_{ac}$ , which is the ac reactance of the wire



# **ac resistance per unit length of a coaxial cable:**

We can find the ac resistance of a coaxial cable made of a central solid round conductor and a coaxial annular conductor surrounding it with a dielectric medium filling the region between the conductors by extending the analysis presented for a straight round wire. For a good conductor making the coaxial cable and at high frequencies, as in the case of a straight wire, we can treat the inner and outer conductors behave as a planar surface.

(ac resistance of a coaxial cable of length *l*) *l* , *a l R*  $\sigma\delta$  2 $\pi$ 1  $\sigma_{\rm ac} = \frac{1}{1-\sigma^2} \frac{t}{2-\sigma}$  (recalled expression for the ac resistance of length *l* of a straight round wire) *a l R*  $\sigma\delta$  2 $\pi$ 1  $_{ac}$  = Concept of finding the ac resistance of a straight wire extended to the inner conductor of radius *a* and to the outer conductor of radius *b* (ac resistance contributed by the inner conductor of length *l*) *b l R*  $\sigma\delta$  2 $\pi$ 1  $_{ac}$  = (ac resistance contributed by the outer conductor of length *l*) *b*  $2\pi\sigma \delta$  | *a b l a l*  $R_{ac} = \frac{1}{\sigma \delta} \frac{l}{2\pi a} + \frac{1}{\sigma \delta} \frac{l}{2\pi b} = \frac{1}{2\pi \sigma \delta} \left| \frac{1}{a} + \frac{1}{b} \right|$  $\int$  $\setminus$  $\overline{\phantom{a}}$  $\setminus$ ſ  $=\frac{1}{2}+\frac{1}{2}+\frac{1}{2}=\frac{1}{2}+\frac{1}{2}$ 1 1 2 1 2 1 2  $\sigma_{\rm ac} = \frac{1}{\sigma \delta} \frac{l}{2\pi a} + \frac{1}{\sigma \delta} \frac{l}{2\pi b} = \frac{1}{2\pi \sigma \delta}$  $\overline{\phantom{a}}$  $\setminus$  $\overline{\phantom{a}}$ ſ  $= 1$ ) of a coaxial cable =  $\frac{1}{2}$  + *a b l* 1 1 2 1 Resistance per unit length  $(l = 1)$  of a coaxial cable

38

 $\int$ 

 $\setminus$ 

 $\pi\sigma\ \delta$ 

*Wave propagation through sea water*

The objective of the study is to find out which frequencies of operation (lower  $\sim$  10 kHz or higher ~ 10 GHz) should be preferred from the standpoint of a lower attenuation of the wave propagating through sea water.

Maxwell's equations (recalled):

$$
\nabla \times \vec{E} = -\mu_0 \frac{\partial \vec{H}}{\partial t} \qquad \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}
$$
\n
$$
\nabla \times \vec{H} = \vec{J} \qquad \qquad \vec{J} = \sigma \vec{E} + \frac{\partial \vec{D}}{\partial t} = \sigma \vec{E} + \varepsilon \frac{\partial \vec{E}}{\partial t}
$$
\n
$$
\nabla \times \vec{H} = \sigma \vec{E} + \varepsilon \frac{\partial \vec{E}}{\partial t}
$$
\n
$$
39
$$

 $\sqrt{v} \times \frac{\partial u}{\partial t} = -\mu_0 \frac{\partial}{\partial t} (\nabla \times H)$   $\longleftarrow$   $\nabla \times H = \partial E + \varepsilon \frac{\partial E}{\partial t}$  (Maxwell's equations)<br>  $\frac{\partial}{\partial t} (\partial \vec{E} + \varepsilon \frac{\partial \vec{E}}{\partial t})$ <br>  $\frac{\partial}{\partial t} = j\omega$ <br>  $\qquad = -j\omega\mu_0 \partial \vec{E} - \mu_0 \varepsilon (j\omega)(j\omega) \vec{E}$ <br>  $\qquad = -j\omega\mu_0 (\sigma + j\omega$ *t*  $\int_0^1 \frac{\partial f}{\partial t}$ *H E*  $\rightarrow$  $\rightarrow$  $\rightarrow$  $\nabla \times$  $\partial$  $\partial$ = −  $\partial$  $\partial$  $\nabla \times \nabla \times \vec{E} = -\mu_0 \nabla \times \frac{\partial H}{\partial x} = -\mu_0$ *t E*  $H = \sigma E$  $\partial$  $\partial$  $\nabla \times H = \sigma E +$  $\rightarrow$  $\rightarrow$  $\vec{\sigma E}+\varepsilon \stackrel{UE}{=}-$  (Maxwell's equations)  $\int_{0}^{C} \frac{\partial E}{\partial t} + \varepsilon \frac{\partial E}{\partial t}$ *t E E t E*  $\partial$  $\partial$ +  $\partial$  $\partial$  $\nabla \times \nabla \times E = \rightarrow$  $\rightarrow$   $\partial$   $\rightarrow$  $\mu_0 = (\sigma E + \varepsilon)$  $E$ **)** $-\nabla^2 \vec{E} = -j\omega\mu_0\sigma\vec{E} - \mu_0 \varepsilon(j\omega)(j\omega)\vec{E}$  $\rightarrow$   $\rightarrow$   $\rightarrow$  $\nabla (\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = -j \omega \mu_0 \sigma \vec{E} - \mu_0 \varepsilon (j \omega) (j \omega)$ *j t* =  $\partial$  $\partial$  $(\vec{E})-\nabla^2\vec{E}=-j\omega\mu_0(\sigma+j\omega\varepsilon)\vec{E}$  $\rightarrow$   $\rightarrow$  $\nabla(\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = -j\omega\mu_0(\sigma + j\omega\varepsilon)\vec{E}$   $\longleftarrow$   $\nabla \cdot \vec{E} = 0$  $\nabla \cdot \vec{E} = 0$ RF quantities vary as  $\exp j(\omega t - \beta z)$  $\vec{E} = j\omega\mu_0(\sigma + j\omega\varepsilon)\vec{E} = \gamma^2\vec{E}$  $\vec{F}$  =  $i\omega U(\sigma + i\omega c)\vec{F}$  =  $\nu^2\vec{F}$ 0  $\nabla^2 \vec{E} = j \omega \mu_0 (\sigma + j \omega \varepsilon) \vec{E} = \gamma$  $\gamma = \sqrt{j\omega\mu_0(\sigma + j\omega\varepsilon_0)} = \alpha + j\beta$ *t H E*  $\partial$  $\partial$  $\nabla \times \vec{E} = \rightarrow$  $\rightarrow$  $\mu_0 \frac{\sigma}{\gamma}$  (Maxwell's equations) Partial time derivative and curl involving partial derivatives with respect to space coordinates are interchangeable

$$
\nabla^2 \vec{E} = j \omega \mu_0 (\sigma + j \omega \varepsilon) \vec{E} = \gamma^2 \vec{E}
$$
\n
$$
\gamma = \sqrt{j \omega \mu_0 (\sigma + j \omega \varepsilon)} = \alpha + j \beta
$$
\n
$$
\frac{\partial^2 E_{x,y}}{\partial x^2} + \frac{\partial^2 E_{x,y}}{\partial y^2} + \frac{\partial^2 E_{x,y}}{\partial z^2} = \gamma^2 E_{x,y} \qquad \frac{\partial}{\partial x} = \frac{\partial}{\partial y} = 0
$$
\n(uniform plane wave supposedly propagating along z)

\n
$$
\frac{\partial^2 E_{x,y}}{\partial x^2} = \gamma^2 E_{x,y} \qquad \gamma = \sqrt{j \omega \mu_0 (\sigma + j \omega \varepsilon)} = \alpha + j \beta
$$
\n
$$
\downarrow
$$
\n<

$$
E_{x,y} = \hat{E}_{x,y} \exp(-\gamma z) = \hat{E}_{x,y} \exp[-(\alpha + j\beta)]z = \hat{E}_{x,y} \exp(-\alpha z) \exp(-j\beta z)
$$

Let us examine two situations: one for  $\sigma > \omega \varepsilon$  and the other for  $\sigma << \omega \varepsilon$  with reference to sea-water communication.

$$
\varepsilon = 81\varepsilon_0 = 81 \times 8.854 \times 10^{-12} \text{ F/m} \qquad \text{(sea water)}
$$
\n
$$
\sigma = 4 \text{ mho/m}
$$

Two alternative ways of putting the propagation constant  $\gamma$ 

$$
\gamma = \sqrt{j\omega\mu_0(\sigma + j\omega\varepsilon)} = \alpha + j\beta
$$

$$
\gamma = \sqrt{j\omega\mu_0\sigma(1 + \frac{j\omega\varepsilon}{\sigma})} = \alpha + j\beta \qquad \gamma = j\omega\sqrt{\mu_0\varepsilon}(1 + \frac{\sigma}{j\omega\varepsilon})^{1/2}
$$

**<u>Propagation at lower frequencies</u>**  $f = 10$  kHz  $= 10 \times 10^3$  Hz (typically )

$$
E_{x,y} = \hat{E}_{x,y} \exp(-\gamma z) = \hat{E}_{x,y} \exp[-(\alpha + j\beta)]z = \hat{E}_{x,y} \exp(-\alpha z) \exp(-j\beta z)
$$

$$
\frac{\omega \varepsilon}{\sigma} = \frac{2\pi f \varepsilon}{\sigma} \approx 1.1 \times 10^{-5}
$$

Let us recall the following expression at lower frequencies:

$$
\gamma = \sqrt{j\omega\mu_0\sigma(1 + \frac{j\omega\varepsilon}{\sigma})} = \alpha + j\beta
$$

$$
f = 10 \text{ kHz} = 10 \times 10^{3} \text{ Hz (typically )}
$$
  
\n
$$
\varepsilon = 81\varepsilon_{0} = 81 \times 8.854 \times 10^{-12} \text{ F/m}
$$
  
\n
$$
\sigma = 4 \text{ mho/m}
$$
 (sea water)

$$
\gamma = \sqrt{j\omega\mu_0\sigma(1 + \frac{j\omega\epsilon}{\sigma})} = \alpha + j\beta
$$
 (recalled at lower frequencies)  
\n
$$
f = 10 \text{ kHz} = 10 \times 10^3 \text{ Hz (typically)}
$$
\n
$$
\frac{\omega\epsilon}{\sigma} = \frac{2\pi f\epsilon}{\sigma} \approx 1.1 \times 10^{-5} \text{ (recalled)}
$$
\n
$$
\epsilon = 81\epsilon_0 = 81 \times 8.854 \times 10^{-12} \text{ F/m}
$$
\n(sea water)  
\nlgnoring the second term under the radical)  
\n
$$
\gamma = \sqrt{j\omega\mu_0\sigma} = \alpha + j\beta
$$
 (separating the real and imaginary parts)  
\n
$$
\alpha_{\text{If}} = \beta_{\text{If}} = \sqrt{\frac{\omega\mu_0\sigma}{2}}
$$
 (recalled)  
\n(obtained by separating the real and imaginary parts)  
\nsubscript if refering to lower frequencies)

**Propagation at higher frequencies**  $f = 10 \text{ GHz} = 10 \times 10^9 \text{ Hz}$  (typically)

Let us recall the following expression at higher frequencies:

1

$$
\gamma = j\omega\sqrt{\mu_0 \varepsilon} (1 + \frac{\sigma}{j\omega \varepsilon})^{1/2}
$$
\n
$$
f = 10 \text{ GHz} = 10 \times 10^9 \text{ Hz}
$$
\n
$$
\sigma = 81\varepsilon_0 = 81 \times 8.854 \times 10^{-12} \text{ F/m}
$$
\n
$$
\sigma = 4 \text{ mho/m}
$$
\n(sea water)  
\n
$$
\gamma = j\omega\sqrt{\mu_0 \varepsilon} (1 + \frac{1}{2} \frac{\sigma}{j\omega \varepsilon}) = \alpha + j\beta
$$
\n
$$
j\omega\sqrt{\mu_0 \varepsilon} + \frac{\sigma}{2} \sqrt{\frac{\mu_0}{\varepsilon}} = \alpha_{\text{hf}} + j\beta_{\text{hf}}
$$
\n(subscript 'hf' referring to quantities at higher frequencies)

$$
\gamma = j\omega \sqrt{\mu_0 \varepsilon} \left(1 + \frac{1}{2} \frac{\sigma}{j\omega \varepsilon}\right) = \alpha + j\beta
$$
  

$$
j\omega \sqrt{\mu_0 \varepsilon} + \frac{\sigma}{2} \sqrt{\frac{\mu_0}{\varepsilon}} = \alpha_{\text{hf}} + j\beta_{\text{hf}}
$$
 (subscript 'hf' referring to quantities at higher frequencies)

$$
j\omega\sqrt{\mu_0\varepsilon} + \frac{\sigma}{2}\sqrt{\frac{\mu_0}{\varepsilon}} = \alpha_{\text{hf}} + j\beta_{\text{hf}}
$$
  
\n
$$
\frac{\alpha_{\text{hf}}}{\alpha_{\text{hf}}} = \frac{\sqrt{\frac{\omega\mu_0\sigma}{2}}}{\frac{\sigma}{2}\sqrt{\frac{\mu_0}{\varepsilon}}} = \sqrt{\frac{2\omega\varepsilon}{\sigma}} = \sqrt{\frac{2\omega_{\text{lf}}\varepsilon}{\sigma}} = \sqrt{\frac{2\omega_{\text{rf}}\varepsilon}{\frac{\sigma}{\sigma}}}
$$
  
\n
$$
\frac{\alpha_{\text{hf}}}{\alpha_{\text{hf}}} = \frac{\sqrt{\frac{\omega\mu_0\sigma}{\mu_0}}}{\frac{\omega_{\text{lf}}}{\varepsilon}} = \sqrt{\frac{2\omega\varepsilon}{\sigma}} = \sqrt{\frac{2\omega_{\text{rf}}\varepsilon}{\frac{\sigma}{\sigma}}}
$$
  
\n
$$
f = 10 \text{ kHz} = 10 \times 10^3 \text{ Hz (lower frequency, typically)}
$$
  
\n
$$
\frac{\alpha_{\text{hf}}}{\alpha_{\text{hf}}} \approx 10^{-3}
$$
  
\n
$$
\frac{\alpha_{\text{hf}}}{\alpha_{\text{hf}}} = \frac{81\varepsilon_0 - 81 \times 8.854 \times 10^{-12} \text{ F/m}}{\sigma = 4 \text{ mho/m}}
$$
  
\n(sea water)  
\n
$$
\lambda = \frac{2\pi}{\beta_{\text{lf}}} = \frac{2\pi}{\sqrt{\frac{\omega\mu_0\sigma}{2}}} = 2\pi \sqrt{\frac{2}{\omega\mu_0\sigma}} = 2\pi \sqrt{\frac{2}{\omega\mu_0\sigma}} = 2\pi \sqrt{\frac{\omega_{\text{min}}}{\omega\mu_0\sigma}} = \sqrt{\frac{\omega\mu_0\sigma}{2}}
$$
  
\nLower frequencies are preferred to higher frequencies for sea-water communication for four attenuation to lower atte.

Lower attenuation at lower frequencies than at higher frequencies

$$
\lambda = \frac{2\pi}{\beta_{\text{lf}}} = \frac{2\pi}{\sqrt{\frac{\omega\mu_0\sigma}{2}}} = 2\pi \sqrt{\frac{2}{\omega\mu_0\sigma}} (= 2\pi\delta_{\text{skin}}) \approx 15 \text{ m}
$$

Lower frequencies are preferred to higher frequencies for sea-water communication for lower attenuation as well as for a reasonable antenna size typically of the order of half wavelength in sea water (as

*Wave propagation in a medium of charged particles*

*Plasma oscillation Refractive index of ionosphere Space-charge waves on an electron beam Cyclotron waves on an electron beam*

*Plasma oscillation*

Consider an ensemble of electrons and positive ions maintaining overall charge neutrality

Consider the physical displacement (perturbation) of electrons (which are much more mobile than positive ions) from their equilibrium position to a small extent

Space-charge electric field in the direction of the displacement of negatively charged electrons  $\implies$  providing a restoring force  $\Rightarrow$ 

Overshoot of electrons

Restoring force again coming into play

 $\Rightarrow$ 

Oscillation of electrons about their mean position at the natural angular frequency― electron plasma frequency.

Displacement of electron layers by an amount  $\xi$  and the resulting space-charge restoring force





$$
\frac{d^2 \xi}{dt^2} = -\omega_p^2 \xi \qquad (\omega_p = \sqrt{\frac{|\eta||\rho_0|}{\varepsilon_0}})
$$
  
\nSolving  
\n
$$
\xi = A \exp(j\omega_p t) + B \exp(-j\omega_p t) \quad (A \text{ and } B \text{ are constants})
$$
  
\n
$$
\xi = A(\cos \omega_p t + j \sin \omega_p t) + B(\cos \omega_p t - j \sin \omega_p t) = (A + B)\cos \omega_p t + j(A - B)\sin \omega_p t
$$
  
\n
$$
\xi = C \cos \omega_p t + D \sin \omega_p t
$$
  
\n
$$
\xi = C \cos \omega_p t + D \sin \omega_p t
$$
  
\n
$$
\xi = 0 \text{ at } t = 0 \longrightarrow C = 0
$$
  
\n
$$
\xi = D \sin \omega_p t
$$

Solution indicating that the electrons oscillate about their mean position with an angular frequency of oscillation  $\omega_p$  called the plasma frequency (electron):

$$
\boldsymbol{\omega}_p\text{=}\sqrt{\frac{\left|\eta\right|\hspace{-1.5mm}\left|\rho_0\right|}{\varepsilon_0}}
$$

*Refractive index of ionosphere*

The ionosphere is located at the heights of 50-300 km from the earth.

The ionosphere consists of electrons and ions

The ionization in the ionosphere is caused by solar radiation (ultraviolet, soft X-ray,  $\alpha$ -particle (helium atoms from which the electrons are knocked off), etc.)

The sky-wave propagation utilizes the phenomenon of total internal reflection from the ionosphere, which, in turn, is dependent on the value of its refractive index.

We can find value of the **refractive index of the ionosphere** by studying the interaction of electromagnetic waves with the ionosphere.

The current density in a medium constituted by charged particles in a free- space medium consists of the convection current density (unlike the conduction current density in a conducting medium) and the displacement current density.



The relation between the convection current density *J*, volume charge density  $\rho$ and velocity *v* of charged particles (electrons) has been obtained earlier (in Chapter 3 while studying Child-Langmuir's law) as:

$$
J=\rho v.
$$

 $J = \rho \vec{v}$ 

 $=\rho^{\frac{1}{2}}$ 

 $\frac{1}{\tau}$   $\rightarrow$ We can write the relation in vector form as

## **Current density equation:**



## **Force equation:**



 $J = \rho_0 \vec{v} + j \omega \varepsilon_0 \vec{E}$ 

 $=\rho_{\rm 0} \vec{v} + j\omega\varepsilon_{\rm 0}\vec{E}\,\,\,\,$  (current density equation)



*Space-charge waves on an electron beam*

It is of interest to study the interaction of electromagnetic waves with a charge flow, for instance, a beam of electrons, which is a constituent of many practical electron devices such as vacuum electron devices like microwave tubes and charge accelerators. We are going to show that an electron beam supports two space-charge waves. Coupling of space-charge waves with electromagnetic waves is of relevance to understanding the behaviour of practical electron devices. Our study will be restricted here to finding the phase velocities of space-charge waves supported by an electron beam.

## **Current density equation**

 $J = \rho v \;$  (convection current density)

=

 $J_0 = \rho_0 v$ 

 $= v<sub>0</sub> +$ 

 $v = v_0 + v$ 

 $_0$  –  $\mu_0$ v<sub>0</sub>

 $\rho_{\scriptscriptstyle (}$ 

 $0^{+1}$ 

 $_0$  +  $P_1$ 

 $0$   $\cdot$   $\cdot$   $1$ 

 $= \rho_0 +$ 

 $= J_0 +$ 

 $J = J_0 + J$ 

Let us consider a large cross-sectional area of the electron beam perpendicular to the beam flow along z over which the beam velocity *v*, volume charge density  $\rho$  and current density  $J$  remain constant:

- One-dimensional beam flow
- $\left[ \rho = \rho_0 + \rho_1 \right]_{\text{Subscript 0}}$  Subscript 0 refers to unperturbed quantities Subscript 1 refers to perturbed quantities

 $\int$  $\left\{ \right.$  $\begin{matrix} \phantom{-} \end{matrix}$  $\partial/\partial z \neq$  $\partial/\partial x = \partial/\partial y =$  $\sqrt{\partial z} \neq 0$  $\frac{\partial}{\partial x} = \frac{\partial}{\partial y} = 0$ *z*  $x = \partial / \partial y$ 

$$
J'_0 + J_1 = (\rho_0 + \rho_1)(v_0 + v_1) = \rho_0 \hat{v}_0 + \rho_0 v_1 + \rho_1 v_0 + \rho_1 v_1
$$
  
\n
$$
J_0 = \rho_0 v_1
$$
  
\n
$$
J_1 = \rho_0 v_1 + \rho_1 v_0 + \rho_1 v_1
$$

 $\overline{1}$  $\left| \right|$ 

 $\overline{ }$  $\overline{ }$ 

 $\vert$ 

 $\left\{ \right.$ 

 $\int$ 

53



54

*v*





**Force equation** Space-charge electric field was introduced in course of the deduction of electron plasma frequency of oscillation in a space-charge neutralised medium consisting of electrons and relatively immobile positive ions. In an ideal vacuum, it is not possible for electrons to move to form an electron beam because of mutual repulsive force between the advancing and the following electrons. However, in a practical vacuum electron beam device like a microwave tube where the vacuum is not ideal, the presence of charge neutralising positive ions makes it possible for the electrons to move and form an electron beam. The space-charge field *E<sup>s</sup>* comes into play for any perturbation in the position of electrons from their equilibrium position.

$$
E_s = \eta E_s \leftarrow \text{ the vacuum is not ideal, the presence of charge neutralising positive ions makes it possible for the electrons to move and form an electron beam. The space-charge field  $E_s$  comes into play for any perturbation in the position of electrons from their equilibrium position. 
$$
\frac{dv_1}{dt} = \frac{\partial v_1}{\partial t} + \frac{dz}{dt} \frac{\partial v_1}{\partial z} = \frac{\partial v_1}{\partial t} + v \frac{\partial v_1}{\partial z} = \frac{\partial v_1}{\partial t} + (v_0 + v_1) \frac{\partial v_1}{\partial z}
$$

$$
= \frac{\partial v_1}{\partial t} + v_0 \frac{\partial v_1}{\partial z} + v_1 \frac{\partial v_1}{\partial z} = \frac{\partial v_1}{\partial t} + v_0 \frac{\partial v_1}{\partial z}
$$
(ignoring higher order term, being the product of perturbed quantities:  $v_1 \partial v_1 / \partial z$ , (to be recalled later in the analysis)
$$

$$
\frac{\partial v_1}{\partial t} + v_0 \frac{\partial v_1}{\partial z} = \eta E_s \qquad \qquad D = \frac{\partial}{\partial t} + v_0 \frac{\partial}{\partial z}
$$
  
 
$$
Dv_1 = \eta E_s \quad \text{(to be recalled later in the analysis)}
$$

(ignoring higher order term, being the product of perturbed quantities:  $v^{}_{\rm l} \partial v^{}_{\rm l}$  /  $\partial z$ 

$$
D\rho_1 = -\rho_0 \frac{\partial v_1}{\partial z} \qquad \text{(recalled)}
$$
\n
$$
\frac{D}{\partial z} = -\rho_0 \frac{\partial v_1}{\partial z} = -\rho_0 \frac{\partial}{\partial z} \frac{\partial v_1}{\partial z} = -\rho_0 \frac{\partial}{\partial z} \frac{\partial v_1}{\partial z} = -\rho_0 \frac{\partial}{\partial z} \frac{\partial}{\partial z} = -\eta \rho_0 \frac{\partial E_s}{\partial z} \qquad [\frac{\partial}{\partial t} + v_0 \frac{\partial}{\partial z} = D]
$$
\n
$$
\frac{(\partial z, \text{ partial derivative with respect to } z, \text{ and } D \text{ involving } \partial/z, \text{ partial derivative with respect to } z, \text{ being interchangeable})}{\text{to } z, \text{ and } \partial t, \text{ partial derivative with respect to } t, \text{ being interchangeable})}
$$
\n
$$
\text{(for a uniform plane wave propagating along } z: \partial/\partial x = \partial/\partial y = 0)
$$
\n
$$
D^2 \rho_1 = -\eta \rho_0 \frac{\partial E_s}{\partial z} \qquad \frac{\partial E_s}{\partial z} = \frac{\rho_1}{\varepsilon_0} \qquad \text{(following from Maxwell's equation: } \nabla \cdot \vec{E} = \frac{\rho}{\varepsilon_0}
$$
\n
$$
D^2 \rho_1 = -\eta \rho_0 \frac{\rho_1}{\varepsilon_0} = -\frac{\eta \rho_0}{\varepsilon_0} \rho_1 = \frac{-|\eta||\rho_0|}{\varepsilon_0} \rho_1 = -\omega_p^2 \rho_1
$$
\n
$$
D^2 = -\omega_p^2 \qquad \frac{|\eta||\rho_0|}{\varepsilon_0} = \omega_p^2 \qquad \frac{|\eta||\rho_0|}{\varepsilon_0} = \omega_p^2 \qquad \omega_p = \sqrt{\frac{|\eta||\rho_0|}{\varepsilon_0}}
$$
\n56





*Cyclotron waves on an electron beam*

An electron beam supports cyclotron waves in the presence of a dc magnetic field in the direction of beam flow, provided there also exist the components of beam velocity transverse to the magnetic field. The interaction of electromagnetic waves with an electron beam supporting cyclotron waves forms the basis of understanding the behaviour of electron beam devices such as the gyrotron for the generation of electromagnetic waves in the millimetre-wave frequency range, which finds application in industrial heating, material processing, plasma heating for thermonuclear power generation as well as in domestic microwave ovens.

Let us consider the electron beam along z and a uniform dc magnetic field present in the region of beam flow, also along z. The components of Lorentz forces exist transverse to the longitudinal magnetic field. Let us treat the problem in rectangular system of coordinates for a large cross-sectional area of the beam perpendicular to the axis of the beam and magnetic field (that is perpendicular to z direction)

$$
\frac{dv_{1x}}{dt} = \frac{e}{m} (\vec{v_1} \times \vec{B})_x = \eta (\vec{v_1} \times \vec{B})_x
$$
\n
$$
\frac{dv_{1y}}{dt} = \frac{e}{m} (\vec{v_1} \times \vec{B})_y = \eta (\vec{v_1} \times \vec{B})_y
$$
\n
$$
\leftarrow \text{subject to Lorentz force}
$$
\n
$$
\frac{dv_1}{dt} = \frac{e}{m} E_s = \eta E_s \text{ (recalled) instead of force due to\nforce equation for an electron\nsubject to space-charge field  $E_s$   
\nforce equation for an electron  
\nsubject to space-charge electric field)
$$

$$
\frac{dv_{1x}}{dt} = \frac{e}{m} (\vec{v}_1 \times \vec{B})_x = \eta (\vec{v}_1 \times \vec{B})_y
$$
\n(recalled)  
\n
$$
\frac{dv_{1y}}{dt} = \frac{e}{m} (\vec{v}_1 \times \vec{B})_y = \eta (\vec{v}_1 \times \vec{B})_y
$$
\n(recalled)  
\n
$$
Dv_{1x} = \eta (\vec{v}_1 \times \vec{B})_x
$$
\n
$$
Dv_{1y} = \eta (\vec{v}_1 \times \vec{B})_y
$$
\n
$$
D = \frac{\partial}{\partial t} + v_0 \frac{\partial}{\partial z}
$$
\n
$$
\vec{v}_1 \times \vec{B} = \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ v_{1x} & v_{1y} & v_{1z} \\ v_{2x} & v_{2x} & v_{2x} \end{vmatrix}
$$
\n
$$
D = \frac{\partial}{\partial t} + v_0 \frac{\partial}{\partial z}
$$
\n
$$
\vec{v}_1 \times \vec{B} = \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ v_{1x} & v_{1y} & v_{1z} \\ v_{2x} & v_{2x} & v_{2x} \end{vmatrix}
$$
\n
$$
Dv_{1x} = \eta Bv_{1x} = -\omega_c v_{1x}
$$
\n
$$
Dv_{1y} = -\eta Bv_{1x} = \omega_c v_{1x}
$$
\n
$$
Dv_{2y} = -\eta Bv_{1x} = \omega_c v_{1x}
$$
\n
$$
Dv_{2y} = -\eta Bv_{1x} = \omega_c v_{1x}
$$
\n
$$
Dv_{2y} = -\eta Bv_{1x} = \omega_c v_{1x}
$$
\n
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Dv_{2y} = -\eta Bv_{1x} = \omega_c v_{1x}
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Dv_{2y} = -\eta Bv_{1x} = \omega_c v_{1x}
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$$
Dv_{2y} = -\eta Bv_{1x} = \omega_c v_{1x}
$$
\n
$$
Dv_{2y} = -\eta Bv_{1x} = \omega_c v_{1x}
$$
\n
$$
Dv_{
$$



$$
\omega - \beta v_0 \mp \omega_c = 0
$$

(Dispersion relation for cyclotron waves)

 $= 0$   $\omega - \beta v_0 = \pm \omega_p$ (Dispersion relation for space-charge waves)

Following the same approach we can write the phase velocities of cyclotron waves simply by replacing  $\omega_p$  with  $\omega_c$ 

$$
v_p = \left(\frac{\omega}{\omega - \omega_c}\right) v_0 > v_0
$$
\n(phase velocity of fast cyclotron wave)

and

$$
v_p = \left(\frac{\omega}{\omega + \omega_c}\right) v_0 < v_0
$$

(phase velocity of slow cyclotron wave)

Led earlier to the derivation of the phase velocities of fast and slow space-charge waves



and

$$
v_p = \left(\frac{\omega}{\omega + \omega_p}\right) v_0 < v_0
$$

(phase velocity of slow space-charge wave)

## **Space-charge and cyclotron waves**



#### Upper sign for the fast wave and lower sign for the slow wave

*Summarising Notes*

 $\checkmark$  Wave equations—one in electric field and the other in magnetic field—have been derived with the help of those two Maxwell's equations in which these field quantities are coupled.

 $\checkmark$  Solutions to the wave equations in electric and magnetic fields have been obtained for uniform, plane electromagnetic waves propagating through an unbounded free-space medium.

✓With the help of Maxwell's equations and the solutions to wave equations in electric and magnetic fields, it has been established, with reference to uniform, plane electromagnetic waves propagating through an unbounded free-space medium, that

 $\Diamond$  there exists no components of electric and magnetic fields in the direction of propagation;

 directions of the electric field, magnetic field and wave propagation are mutually perpendicular to one another;

 transverse electromagnetic (TEM) mode of propagation is supported by the unbounded medium;

 $\Diamond$  intrinsic impedance and phase velocity of the wave are each related to the permeability and the permittivity of free space, the wave phase velocity being the speed of light *c*.

 $\checkmark$  Concepts of the skin depth, surface resistance and ac or RF resistance of a medium have been developed by studying the propagation of uniform, plane electromagnetic waves propagating through a semi-infinite conducting medium, considering such waves to be incident from a free-space region to a planar conducting surface extending to infinity.

✓Ratio of the ac or RF resistance to dc resistance of a conducting wire of circular cross section becomes equal to the ratio of wire radius to twice skin depth, considering the wire to be of high conductivity and/or wave frequencies to be very high such that the skin depth of the conductor becomes small enough compared to the wire radius to make the planar conductor approximation for the conducting wire of circular cross section.

 $\checkmark$  Lower frequencies, say, ~10 kHz is preferred to higher frequencies, say, ~10 GHz, in view of comparatively lower attenuation of waves at such lower frequencies for seawater communication as revealed by studying propagation through unbounded seawater of finite conductivity and permittivity.

 $\checkmark$  Study of wave propagation through a medium of charged particles give the concepts of sky-wave propagations through ionosphere as well as those of space-charge waves and cyclotron waves on an electron beam.

*Readers are encouraged to go through Chapter 6 of the book for more topics and more worked-out examples and review questions.*